

# TIM deposition and characterization\*

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**Usage:** Application of the TIM on the modules of the Dee. After the application, assembly the Dee. The Dee is going to be implemented on the TFPX of CMS, Cern.

## I. INTRODUCTION

The Thermal Interface Material (TIM) is a material, mostly composed of a conductive material that is inserted between two components, it could be between a sensor, CPU or modules and a heat sink enhancing the thermal coupling between them. Mostly the TIM is implemented in systems like computers and sensors to avoid thermal runaway and damaging the components. To explain what is thermal runaway in this system we have to define dark currents. Dark currents is a temperature-dependant current flows into photosensitive devices when not actively being irradiated, in this case the sensors that are in the Dee's. This is due to the random generation of electron and holes within the depletion region of the device, in this case the region that the sensors are in the Dee. It consists of the charges generated in the detector through heat, when no outside radiation is entering the detector. This creates a cycle between the current and dark currents of heat, exponentially escalating temperature creating a thermal runaway and finally damaging all the components.

The TFPX (Tracker Frontal Pixel) it is part of the Inner Tracker of CMS. The TFPX has 8 planar disks that are divided by half, these halves are the Dees.

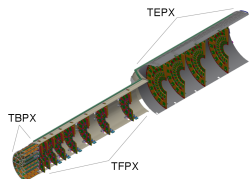


FIG. 1. TFPX

The Dees 2 are currently made of carbon fiber

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and are the ones holding the thermal system and the modules on the CMS TFPX.

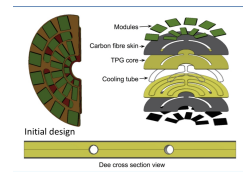


FIG. 2. Dee

The modules are located in the surface of the Dee glued with epoxy.

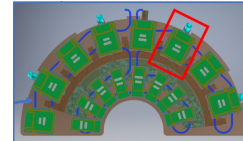


FIG. 3. Location of the modules

The TIM that is used for the modules on the Dee is Moresco + 20 $\mu$ m diamond at 70%.

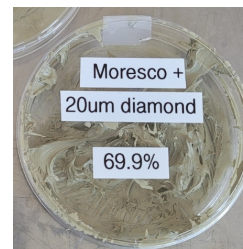


FIG. 4. Moresco + diamond at 70%

This is because according to thermal measurements, the thermal conductivity of the Moresco improves when its mixed with diamonds without suffering radiation damages. In the next image, you can see the thermal conductivity of different concentrations of diamonds with Moresco.

Material	k (W/mK)
Pure Moresco PPE	0.20 ± 0.02
PPE + 33% diamond (20 μm)	0.33 ± 0.03
PPE + 70% diamond (20 μm)	1.17 ± 0.11
PPE + Mixed-diameter diamond	0.78 ± 0.08

FIG. 5. Thermal Conductivity of Moresco

49 According to Souvik's measurements the best  
50 thickness of the Moresco + diamonds is at 100 μm.

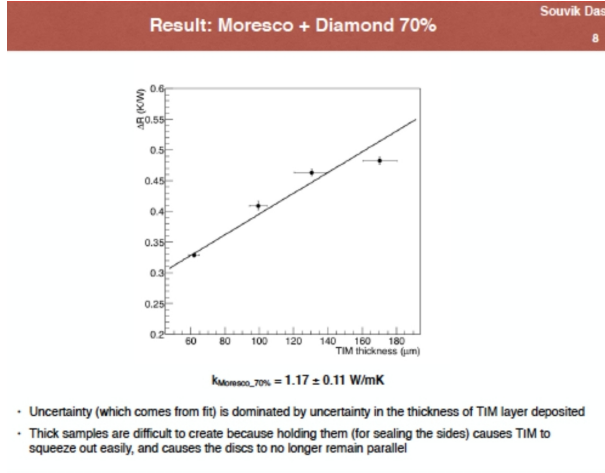


FIG. 6. Best thickness of Moresco

51 To be able to apply the Moresco on the modules,  
52 a double-Y pattern was suggested.

## 53 II. DOUBLE-Y PATTERN

54 The double-Y pattern consists in two parallel lines  
55 on the sides and an overlapping line on the center  
56 as seen on the figure 7.

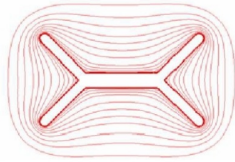


FIG. 7. Double-Y pattern

57 The double-Y pattern was suggested by Jose Mon-  
58 roy to be able to disperse the TIM across the length  
59 and width of the module due to the rectangular  
60 shape of the modules. The technique of doing com-  
61 plex shapes of TIM is widely used to disperse TIM in  
62 electronics such as CPU's, GPU's, and other com-  
63 ponents that requires a material to disperse heat.

64 Usually these components are square shaped  
65 surfaces, that makes easy the task of dispersing the TIM  
66 equally to each corner applying a moderate force in  
67 top of them. In the figure 8 is shown how the scat-  
68 tering of TIM on square surfaces.

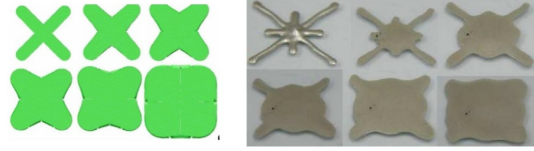


FIG. 8. Scattering of TIM in a CPU

## 69 III. TIM DEPOSITION

70 The TIM deposition was mainly done using a  
71 gantry programmed with LabVIEW. The gantry  
72 itself can be managed by a proprietary program  
73 named Motion Composer, which can move the  
74 gantry to the desired velocity and distance; but to be  
75 able to run routines, include more components such  
76 as cameras, microscopes, etc., and tasks at a desired  
77 time and automatically, its easier to program it with  
78 LabVIEW. The model of the gantry is the Aerotech  
79 A3200.

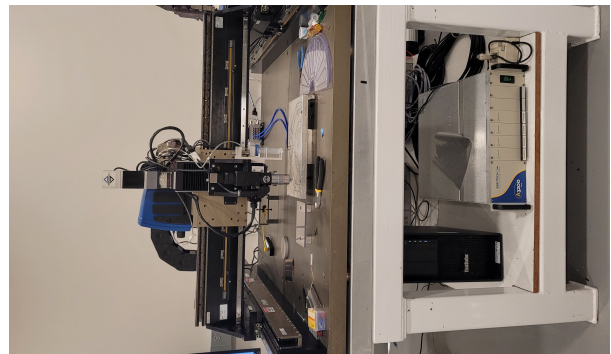


FIG. 9. Aerotech Gantry

To be able to dispense the Moresco + 20 μ dia-  
mond at 70% we used a dispenser from the company  
Nordson. This particular dispenser can push up to  
100psi.

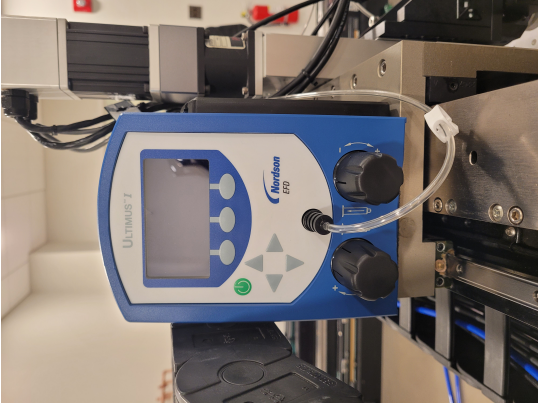


FIG. 10. Dispenser

84 The gantry has an machined attachment made by  
 85 Jose Monroy that holds the syringe on the gantry  
 86 and makes it easier to connect the syringe to the  
 87 dispenser.

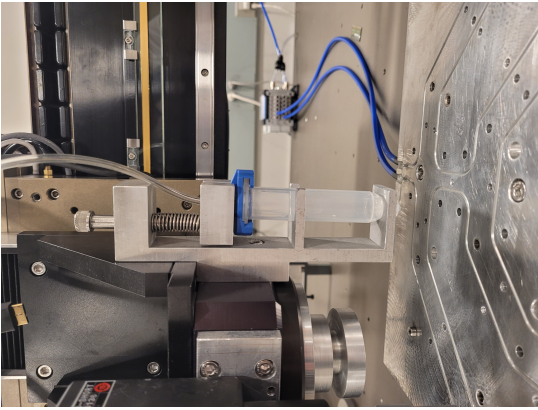


FIG. 11. Syringe attached to the gantry

#### 88 IV. DISPENSING A DOUBLE-Y PATTERN

89 The TIM should spread across the length of the  
 90 ceramic heater that is 35mm x 20mm. This com-107  
 91 ponent is part of the set up for the simulation of a108  
 92 thermal runaway. Using the gantry I was able to109  
 93 map out the key points of the desired length. Doing110  
 94 an approximation of after scattering of 1.5mm, the111  
 95 diagonal lines, named  $l_1$  measures 6.5mm and the112  
 96 straight line in the middle of the double Y, named113  
 97  $l_2$  measures 18.14mm. Finally the angle of the open-114  
 98 ing between the straight line and diagonal line mea-115  
 99 sures 133.1 degrees, the final diagram can be seen116  
 100 on figure 12. Since LabVIEW can move the gantry117  
 101 using distances, I made the LabVIEW program to118  
 102 ask for the initial point for the double-Y and after119  
 103 that adding the MathScript function on LabVIEW I120

104 was able to calculate the remaining points with the  
 105 distances.

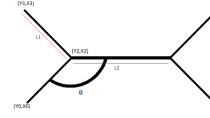


FIG. 12. Points of the double-Y pattern

A very interesting detail to know is that it can be observed that the axis on the figure 12 are backwards. This is because the gantry moves forward in  $X$  and to the sides in  $Y$ . Taking that perspective of viewer (seen in front of the gantry) the double-Y pattern will be seen as it. The way that it was made, was calculating the next point in reference of the initial point:

$$Y_1 = Y_0 \quad (1)$$

$$X_1 = X_0 - 2l_1 \sin \theta \quad (2)$$

$$Y_2 = Y_0 - l_1 \cos \theta \quad (3)$$

$$X_3 = x_0 - l_1 \sin \theta \quad (4)$$

106 The routine for the gantry to move was:

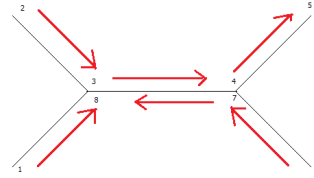


FIG. 13. Movement gantry 1

To dispense the Moresco an olive needle tip was used. This needle tip has an internal circumference of 1.54mm. This needle tip was used because the opening was big enough to pass the Moresco mix and maintaining the precision of the dispensing. When this routine was tested, we saw that the Moresco stretched on the empty spaces of the double-Y pattern. For example on step 4 to 5 was a huge problem. To fix this issue after finishing each line, the Z-axis was lowered to stick the remaining Moresco off the tip of the needle and continue on the routine. After multiple tests, a new routine was thought to decrease the timing that took the gantry to move and avoid the Moresco to stretch (see figure 14).

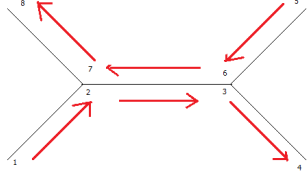


FIG. 14. Movement gantry 2

121 To code this new routine on LabVIEW some few  
122 fixes were done with the equations.

$$\begin{aligned} X_1 &= -l_1 \sin \theta & (5)_{136} \\ Y_1 &= l_1 \cos \theta & (6)_{137} \\ X_2 &= X_1 & (7)_{138} \\ Y_2 &= Y_1 + l_2 & (8)_{140} \\ X_4 &= 2l_1 \sin \theta & (9)_{141} \\ Y_4 &= 0 & (10)_{142} \end{aligned}$$

### 123 A. Double-Y tests

124 On the first sample, took a load cell to measure  
125 how much force required the double-Y to dispense  
126 to the sides. To be able to run the load cell used  
127 an Arduino and exported the data obtained from  
128 it. The numbers are negative because the way the  
129 load cell works, it retrieves the data as pushing as a  
130 negative and pull as a positive.

Time in seconds	Pressure applied
0.0	-0.099 kg
0.5	-0.196 kg
1.0	-0.265 kg
1.5	-0.321 kg
2.0	-0.407 kg
2.5	-0.407 kg
3.0	-0.527 kg
3.5	-0.591 kg
4.0	-0.644 kg
4.5	-0.679 kg
5.0	-0.716 kg
5.5	-0.729 kg
6.0	-0.769 kg
6.5	-0.838 kg
7.0	-0.929 kg
7.5	-0.960 kg
8.0	0.002 kg
8.5	-0.005 kg

134 As you can observe it required a lot of force to be  
135 able to disperse completely to the sides.



FIG. 15. First double Y

Noticing that the modules are very fragile, it is noticeable that using 1kg of force its too much because on the spreading process it potentially break the module on the dee. Using previous knowledge of Phase 1, the maximum force that the modules could withstand was 200g. Knowing this information, more tests were conducted using the measurements of the plaquette for the thermal runaway tests and the measurements of the mock up module. Having in mind that the maximum force applied was 200g. These measurements are:

Measurements	
Plaquette	Mock up Module
35mm x 20mm	40mm x 25mm

To be able to disperse the double-Y pattern uniformly to the edges, a 5 point tool was built using a glass slide and pieces of metal. Later on, a 3D printer version was made with adjustable positions for the screws to be able to test different pressure points for the double-Y pattern.

### 156 B. Results

157 Next, a list of all the test conducted of the  
158 double-Y pattern. Initial measurements for the  
159 short double-Y pattern:

Test	Pressure	Length	Width	Width double line	Thickness	Weight
1	30psi	27.25mm	16.35mm	5.53mm	2.03mm	5.30g
2	30psi	27.51mm	15.29mm	5.65mm	2.17mm	5.20g
3	25psi	26.26mm	14.56mm	5.77mm	2.99mm	-
4	20psi	26.47mm	14.45mm	-	3.66mm	-
5	20psi	25.15mm	14.07mm	2.34mm	2.02mm	-
6	18psi	25.52mm	15.24mm	2.38mm	1.69mm	-
7	16psi	25.07mm	15.59mm	1.83mm	1.80mm	-

After applying 200g:

Test	Length	Width	Thickness
1	30.25mm	17.38mm	0.79mm
2	28.25mm	18.38mm	0.77mm
3	30.31mm	19.40mm	0.91mm
4	31.44mm	18.22mm	0.48mm
5	28.73mm	16.42mm	0.43mm
6	27.44mm	16.25mm	0.56mm
7	26.30mm	17.02mm	0.17mm

165  
166

167 Initial measurements for the double-Y pattern  
168 with the length of the mock up module:

169

Test	Pressure	Length	Width	Width double line	Thickness
1	25psi	38.19mm	15.27mm	5.51mm	3.05mm
2	20psi	39.50mm	14.03mm	2.80mm	2.88mm
3	25psi	37.80mm	14.50mm	3.13mm	1.72mm
4	20psi	37.92mm	14.86mm	2.23mm	1.08mm
5	18psi	36.70mm	13.72mm	1.68mm	0.78mm

170  
171

172 After applying 200g:

173

Test	Length	Width	Thickness
1	42.06mm	19.28mm	1.61
2	41.94mm	15.30mm	0.47mm
3	39.76mm	16.10mm	0.47mm
4	39.82mm	16.16mm	0.14mm
5	39.19mm	16.73mm	0.10mm

174

175 After conducting the tests, you can observe that  
176 on the test 5 of the long double-Y pattern the  
177 double-Y pattern reached the 0.10mm or 100μ thick  
178 but the pattern was severely damaged and it didn't  
179 disperse at all to the sides as you can see on the  
180 figure 16.



FIG. 16. Non-dispersed double-Y pattern

181 Additionally, if we compare the data obtained af-  
182 ter pressing the Moresco mix with a 200g you can  
183 observe that most of them push until 0.40mm thick  
184 if its thicker than 1.00mm.

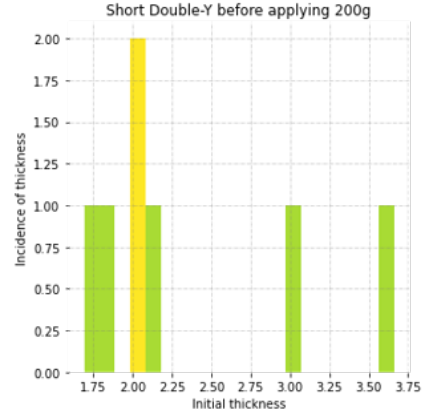


FIG. 17. Short double-Y before applying 200g

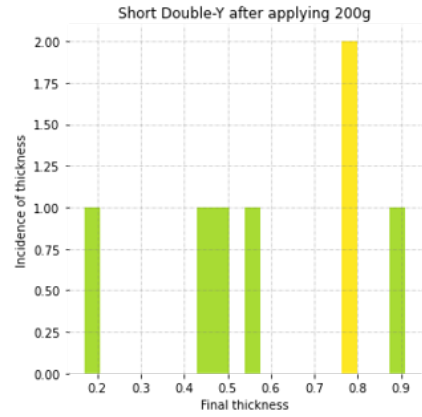


FIG. 18. Short double-Y after applying 200g

185 You can observe on the figure 18 that the inci-  
186 dence of thickness for the short double-Y pattern  
187 are between 0.70mm and 0.80mm. Now for the long  
188 double-Y pattern we have:

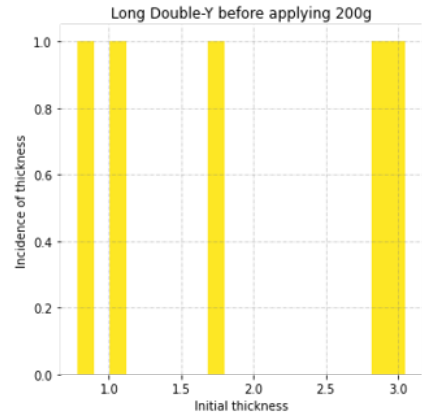


FIG. 19. Long double-Y before applying 200g

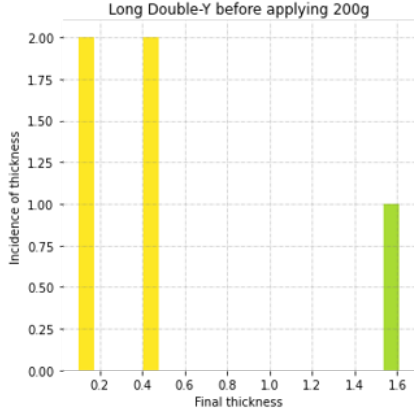


FIG. 20. Long double-Y after applying 200g

189 In this type of double-Y pattern the greater incidence of thickness was 0.4mm even though on the  
 190 other type of double-Y didn't was the case, gathering all the info, the media of the thickness is 0.4mm. So  
 191 that means that the double-Y pattern is not a good shape to disperse in the rectangular space without  
 192 using a lot of force to disperse it. The best way to apply TIM is by doing a ribbon.  
 193  
 194  
 195  
 196

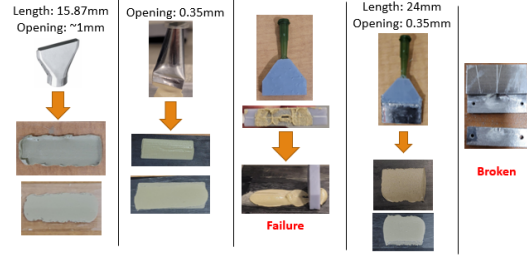


FIG. 21. Ribbon Needles

219 The majority of the discarded needles were mainly  
 220 because they were dispensing the ribbon too thick.  
 221 To be able to achieve a good ribbon with the de-  
 222 sired thickness, the ribbon had to have an opening  
 223 of  $100\mu$ , use a very low pressure and lower the nee-  
 224 dle as close to the surface as possible. The working  
 225 needle is shown on the figure 22

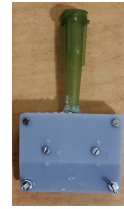


FIG. 22. Working needle tip

## V. RIBBON NEEDLE TIP

197

198 After discarding the double-Y pattern, another  
 199 idea was doing a ribbon. The advantages of the rib-  
 200 bon is that it only needs one routine on the gantry.  
 201 Since we need several modules on the on the dee hav-  
 202 ing less routines on the gantry will guarantee that  
 203 it will take less time dispensing. The doctorate stu-  
 204 dent, Xingchen Fan ordered the ribbon needles from  
 205 China, luckily they arrived at the same week that  
 206 the idea of the double-Y pattern was discarded. To  
 207 perform the test, initially we started off with the 5  
 208 point spreader to disperse it better to the sides.

209 One thing that it was noticeable was that for all  
 210 the test conducted, the Moresco was being recycled.  
 211 In the recycling process the Moresco got contami-  
 212 nated with some dust from the surfaces, and glass  
 213 shards. This made the Moresco more viscous and it  
 214 took more force to push for the tests. New Moresco  
 215 had to be mixed. Moresco with  $20\mu$ ,  $36\mu - 54\mu$ , and  
 216  $54\mu - 80\mu$  diamond was mixed.

217 The ribbon needle tips that were used before find-  
 218 ing the best design were:

226 One thing that was noticeable was bubbles on the  
 227 sample, shown on the figure 23.

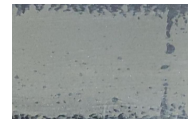


FIG. 23. Bubbles on Moresco sample

228 Initially, it was thought that the bubbles came up  
 229 from the syringe and the deposition, but after ob-  
 230 serving carefully and taking a video these "bubbles"  
 231 were generated by the stretching of the Moresco on  
 232 the surface and due to the low pressure it created  
 233 these holes, not bubbles.

234 To be able to fix this problem, a scraper was in-  
 235 stalled on the back of the needle tip to flatten up the  
 236 surface, achieve the desired thickness and fill these  
 237 holes. The scraper installed on the needle tip can be  
 238 seen on the figure 24.

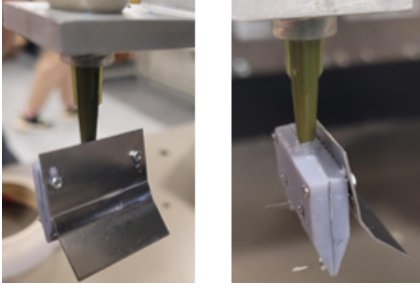


FIG. 24. Scraper installed on the needle tip

239 To install and make the scraper usable, it had to  
 240 be calibrated using the surface as a base and using  
 241 the Z-axis of the gantry, the thickness of the Moresco<sup>271</sup>  
 242 was about the same as the distance of the surface<sup>272</sup>  
 243 from the scraper. After using the scraper, a good<sup>273</sup>  
 244 amount of Moresco was built on the back of it, but<sup>274</sup>  
 245 thankfully was useful to fill the gaps on the sample.<sup>275</sup>

246 Since the gantry has to mass produce, another run  
 247 to do another ribbon was made without cleaning the<sup>276</sup>  
 248 back of the scraper to see if the ribbon was going to<sup>277</sup>  
 249 be damaged, and indeed it was. To solve this issue,<sup>278</sup>  
 250 using a vacuum pump, install on the back of the<sup>279</sup>  
 251 scraper a small tube with an opening. This tube will<sup>280</sup>  
 252 be connected to a small box to collect the Moresco<sup>281</sup>  
 253 and prevent the vacuum pump be damaged by the<sup>282</sup>  
 254 Moresco.<sup>283</sup>

255 Another thing noted was that the surface of the<sup>284</sup>  
 256 sample has to be leveled, otherwise it will have a<sup>285</sup>  
 257 thick side or the scraper can touch the surface and<sup>286</sup>  
 258 damage it. This was observed while dispensing in a

259 sample with the tubes attached to the carbon fiber  
 260 sandwich.

261 Lastly, after dispensing on the carbon-fiber sand-  
 262 wich with the tubes attached, this sample was taken  
 263 to the thermal runaway test to seek if the simulations  
 264 and expectations of the gantry dispensed Moresco  
 265 reach up to the desired temperature. After this step,  
 266 next thing is to perfect the needle tip by making  
 267 the same model in stainless steel and calibrate the  
 268 scraper with the new needle tip, and build the vac-  
 269 uum pump setup.

## VI. REFERENCES

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